

# CS 545 – Lecture 8

## Direct Kinematics

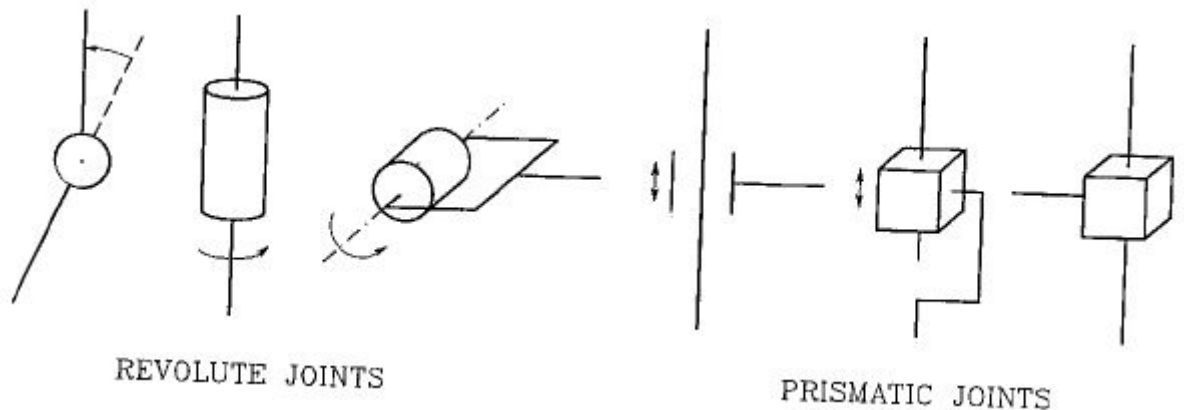
- Transformation from Joint Space to End-effector Space
- Denavit-Hartenberg Convention
- Examples
- Workspace Consideration

<http://robotics.usc.edu/~aatrash/cs545>

# Direct Kinematics



- Manipulator has *links* and *joints*
- *Revolute* and *prismatic* joints

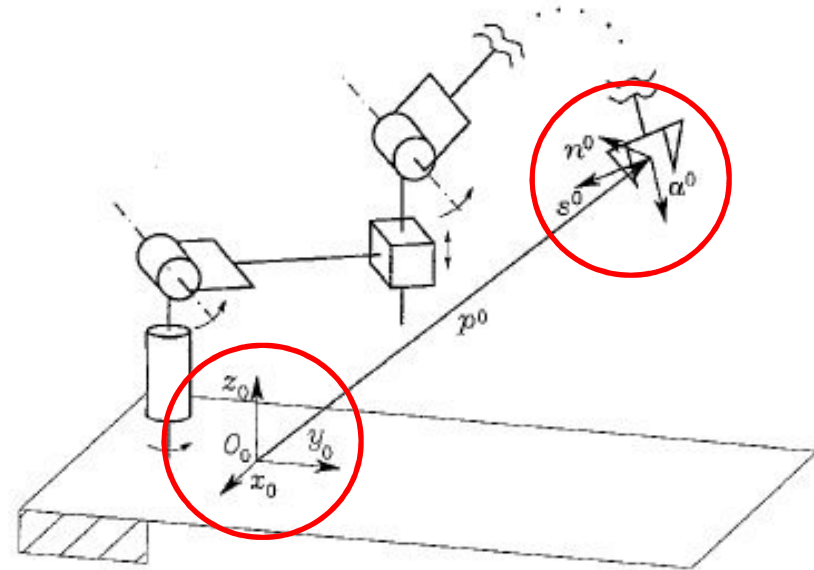


- *Base* and *endeffector*
- Entire structure: *open kinematic chain*

# Direct Kinematics



- *Direct kinematics* – Determine the end effector position and orientation as a function of joint variables
- *End-effector frame*
- *Base frame*

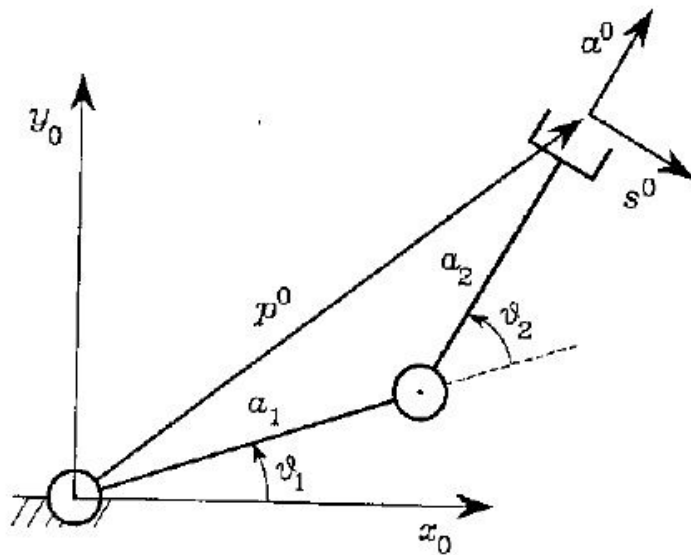


$$T^0(q) = \begin{bmatrix} n^0(q) & s^0(q) & a^0(q) & p^0(q) \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

# Direct Kinematics



- Geometric analysis



$$s_{ij} = \sin(q_i + q_j)$$
$$c_{ij} = \cos(q_i + q_j)$$

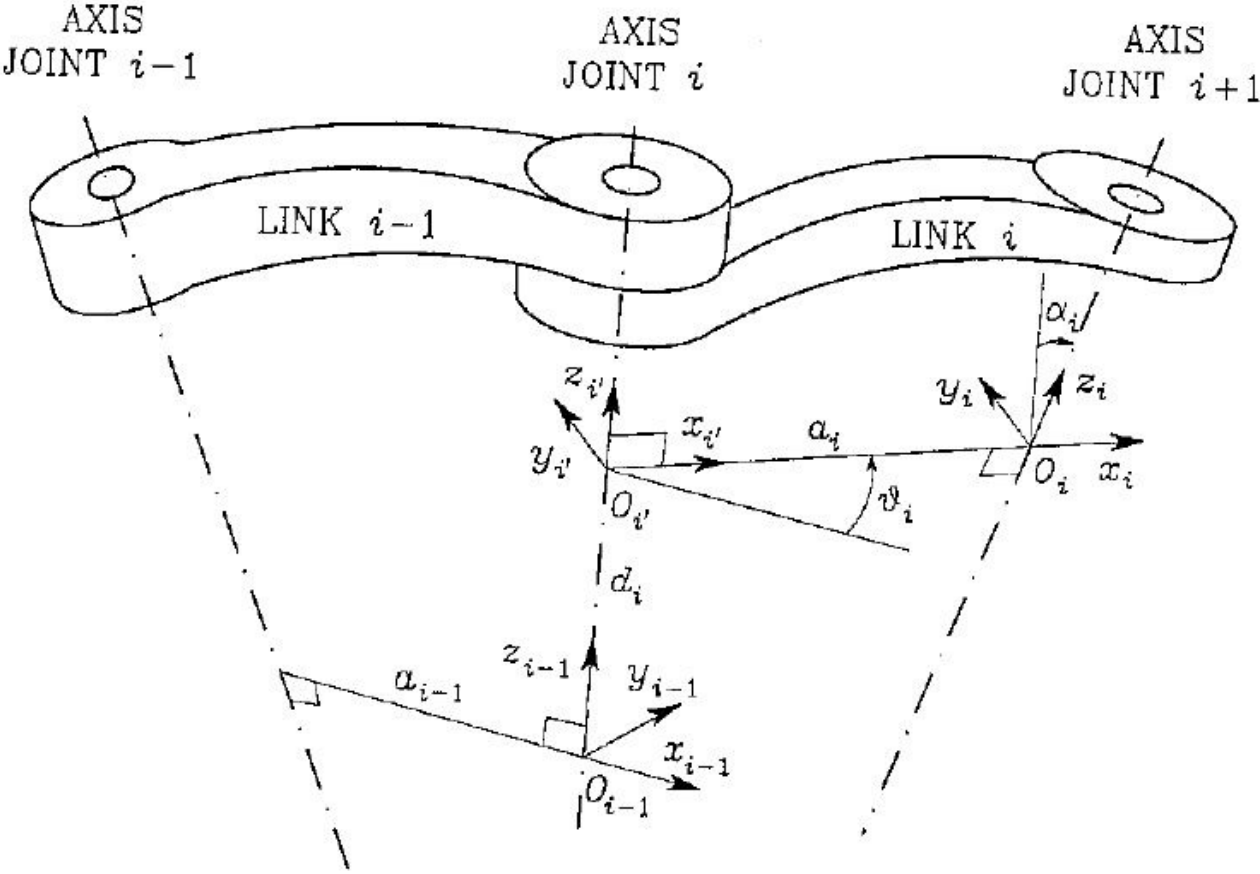
$$T^0(q) = \begin{bmatrix} n^0 & s^0 & a^0 & p^0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0 & s_{12} & c_{12} & a_1 c_1 + a_2 c_{12} \\ 0 & -c_{12} & s_{12} & a_1 s_1 + a_2 s_{12} \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Denavit-Hartenberg Convention



- Assume each joint connects two and only two consecutive links
- Describe this relationship and solve overall description recursively
- Use a set of rules (conventions really) known as *Denavit-Hartenberg Convention*
- (also called *DH Frames*)
- **Goal:** Find transform from link  $i$  to link  $i+1$

# Denavit-Hartenberg Convention

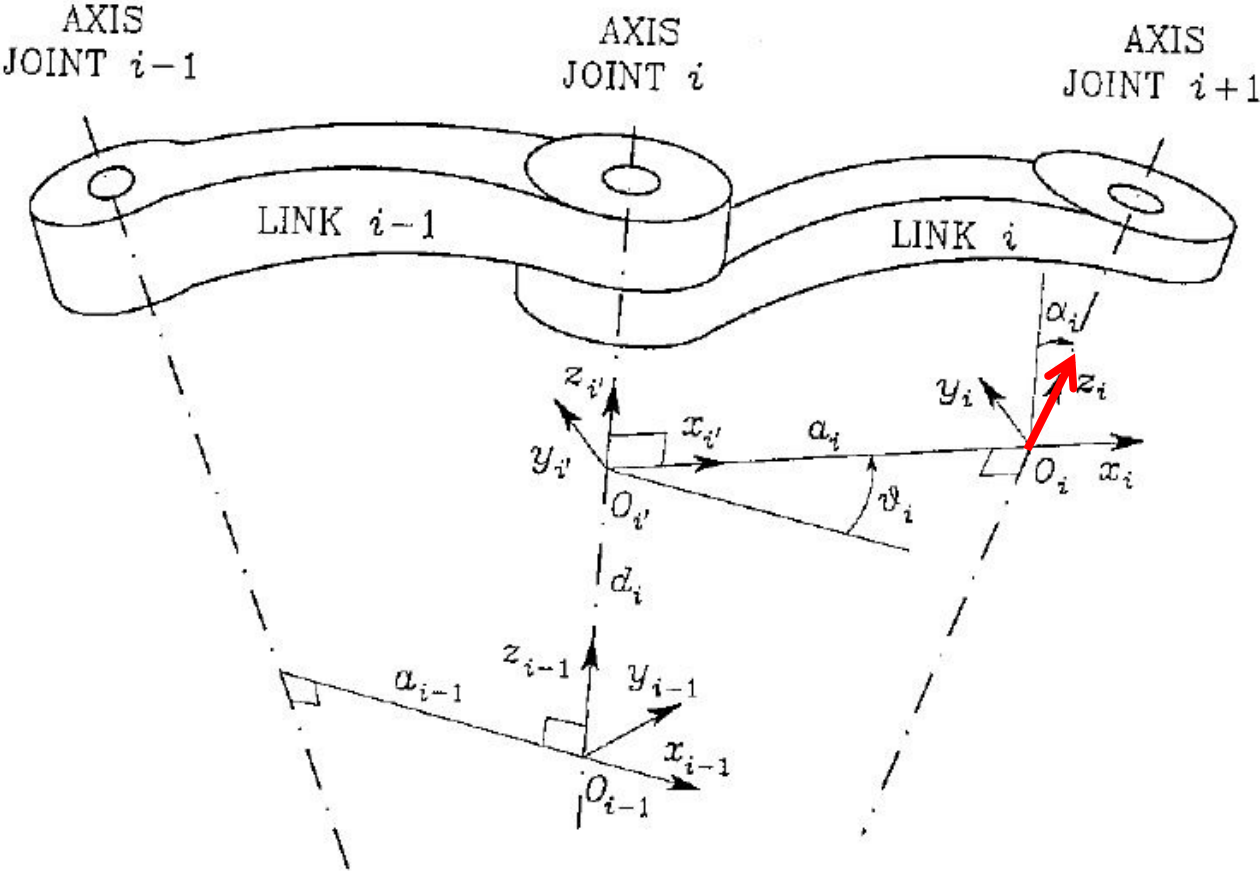


# Denavit-Hartenberg Convention



- Choose axis  $z_i$  along axis of joint  $i+1$
- Location origin  $O_i$  at intersection of  $z_i$  and common normal with  $z_{i-1}$ .
- Location origin  $O_{i'}$  at intersection of  $z_{i-1}$  and common normal with  $z_i$ .
- Choose axis  $x_i$  along common normal to axes  $z_{i-1}$  and  $z_i$
- Choose axis  $y_i$  to complete right-handed frame

# Denavit-Hartenberg Convention



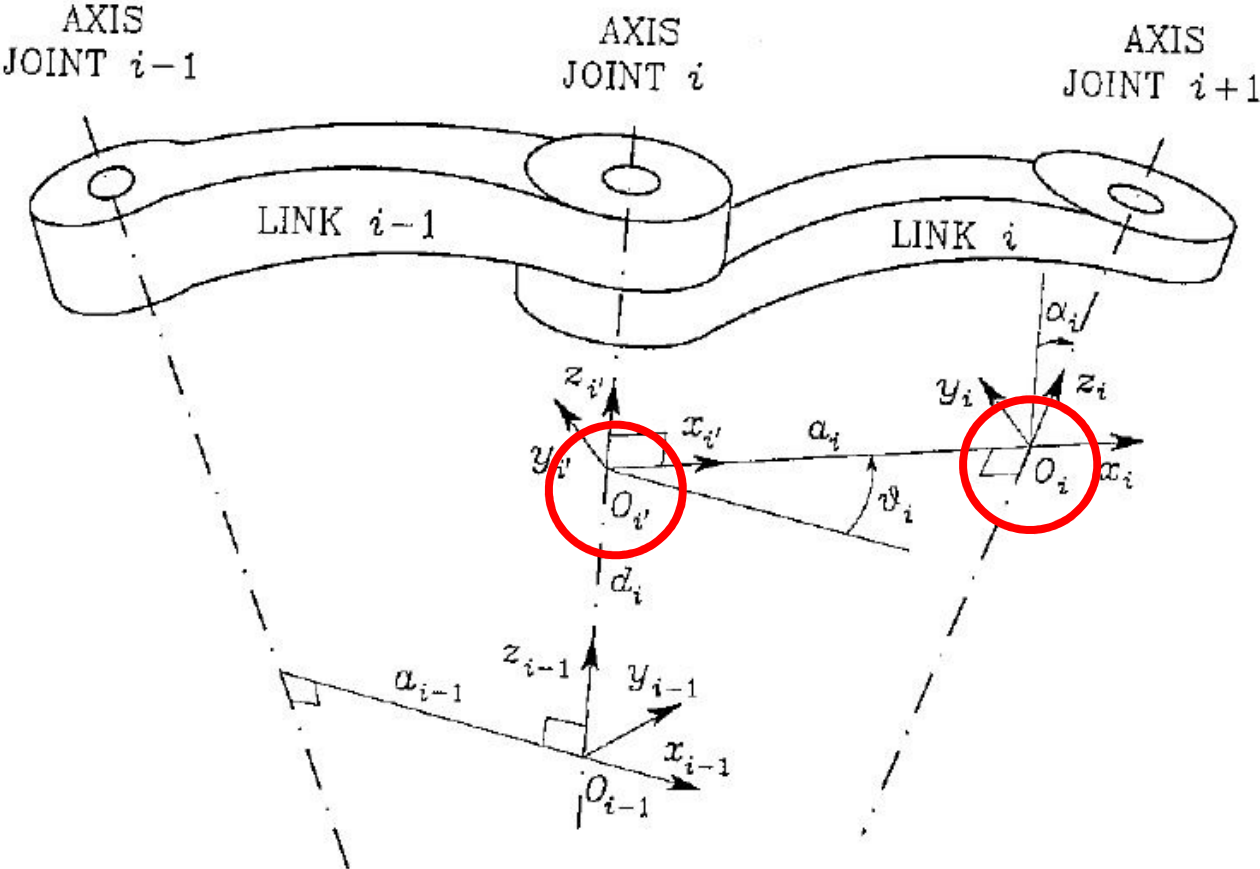


# Denavit-Hartenberg Convention



- Choose axis  $z_i$  along axis of joint  $i+1$
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- Choose axis  $y_i$  to complete right-handed frame

# Denavit-Hartenberg Convention

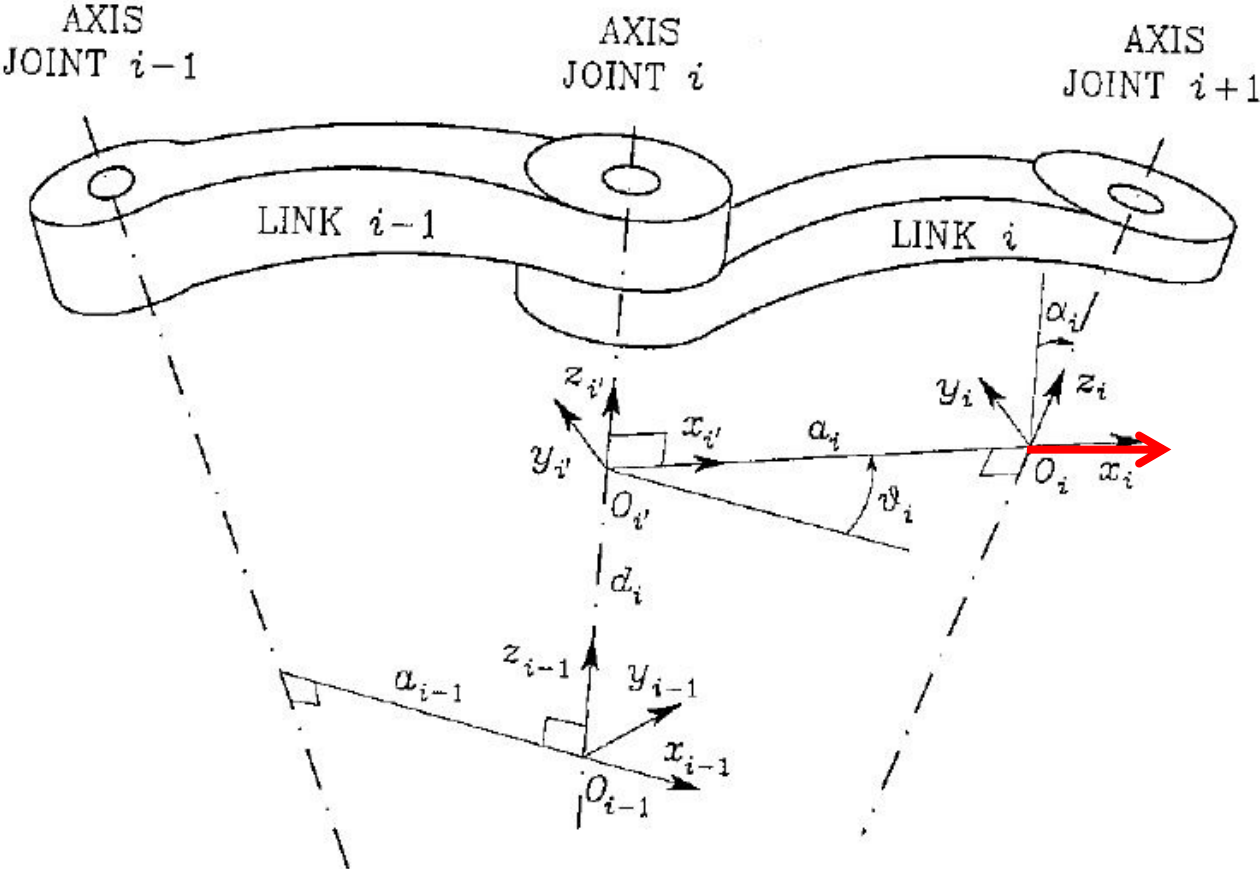


# Denavit-Hartenberg Convention



- Choose axis  $z_i$  along axis of joint  $i+1$
- Location origin  $O_i$  at intersection of  $z_i$  and common normal with  $z_{i-1}$ .
- Location origin  $O_{i'}$  at intersection of  $z_{i-1}$  and common normal with  $z_i$ .
- Choose axis  $x_i$  along common normal to axes  $z_{i-1}$  and  $z_i$
- Choose axis  $y_i$  to complete right-handed frame

# Denavit-Hartenberg Convention

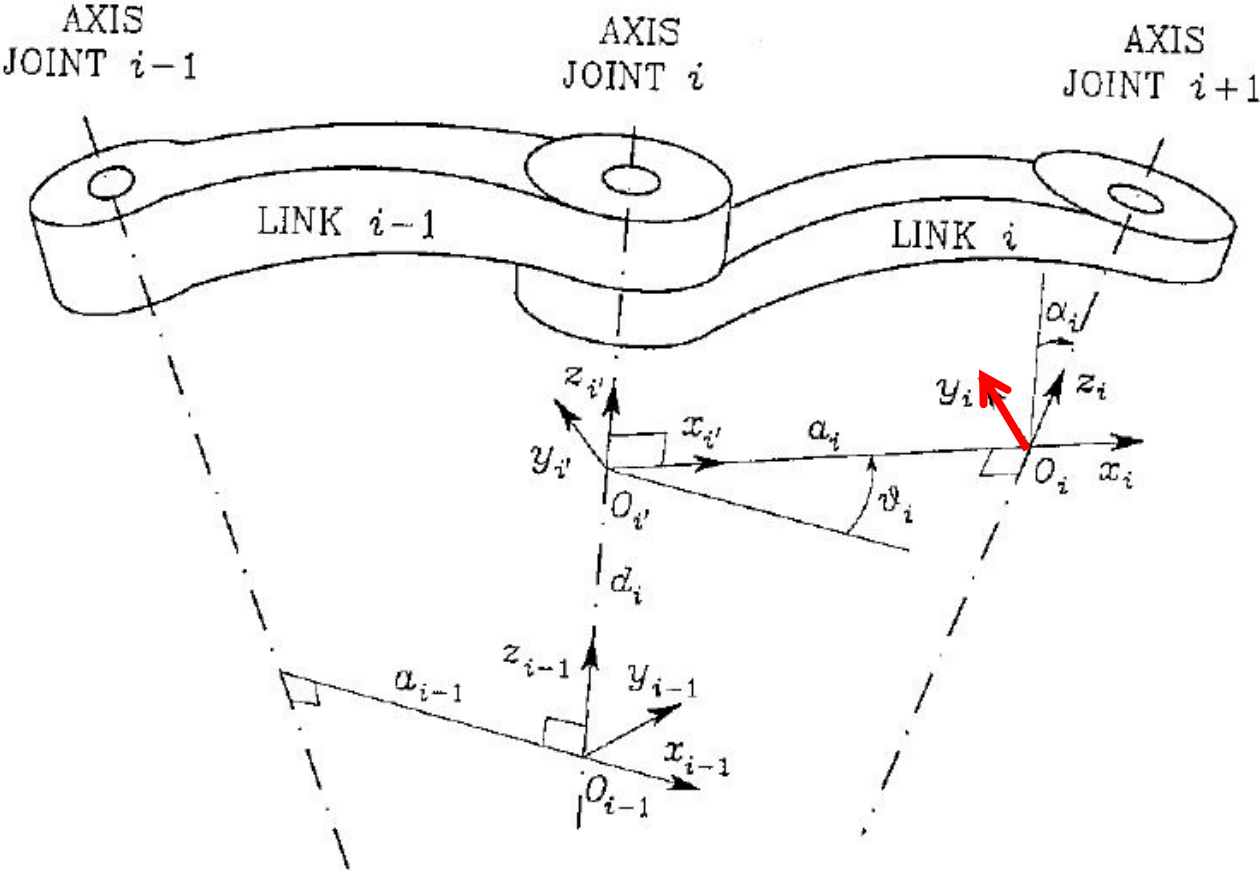


# Denavit-Hartenberg Convention

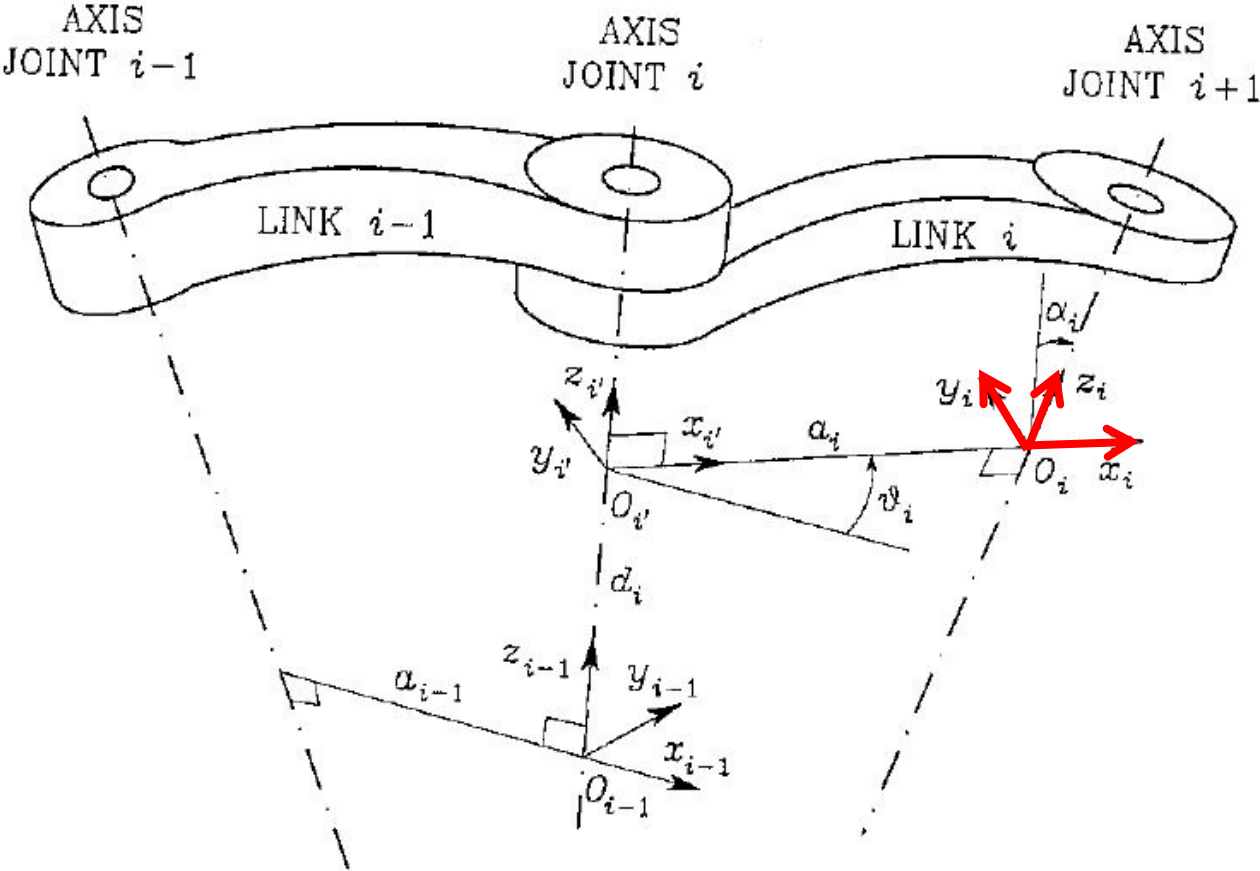


- Choose axis  $z_i$  along axis of joint  $i+1$
- Location origin  $O_i$  at intersection of  $z_i$  and common normal with  $z_{i-1}$ .
- Location origin  $O_{i'}$  at intersection of  $z_{i-1}$  and common normal with  $z_i$ .
- Choose axis  $x_i$  along common normal to axes  $z_{i-1}$  and  $z_i$
- Choose axis  $y_i$  to complete right-handed frame

# Denavit-Hartenberg Convention



# Denavit-Hartenberg Convention



# Denavit-Hartenberg Convention



- Relationship between frame  $i-1$  and frame  $i$  defined by 4 parameters:

$a_i$  distance between  $O_i$  and  $O_{i'}$ ,

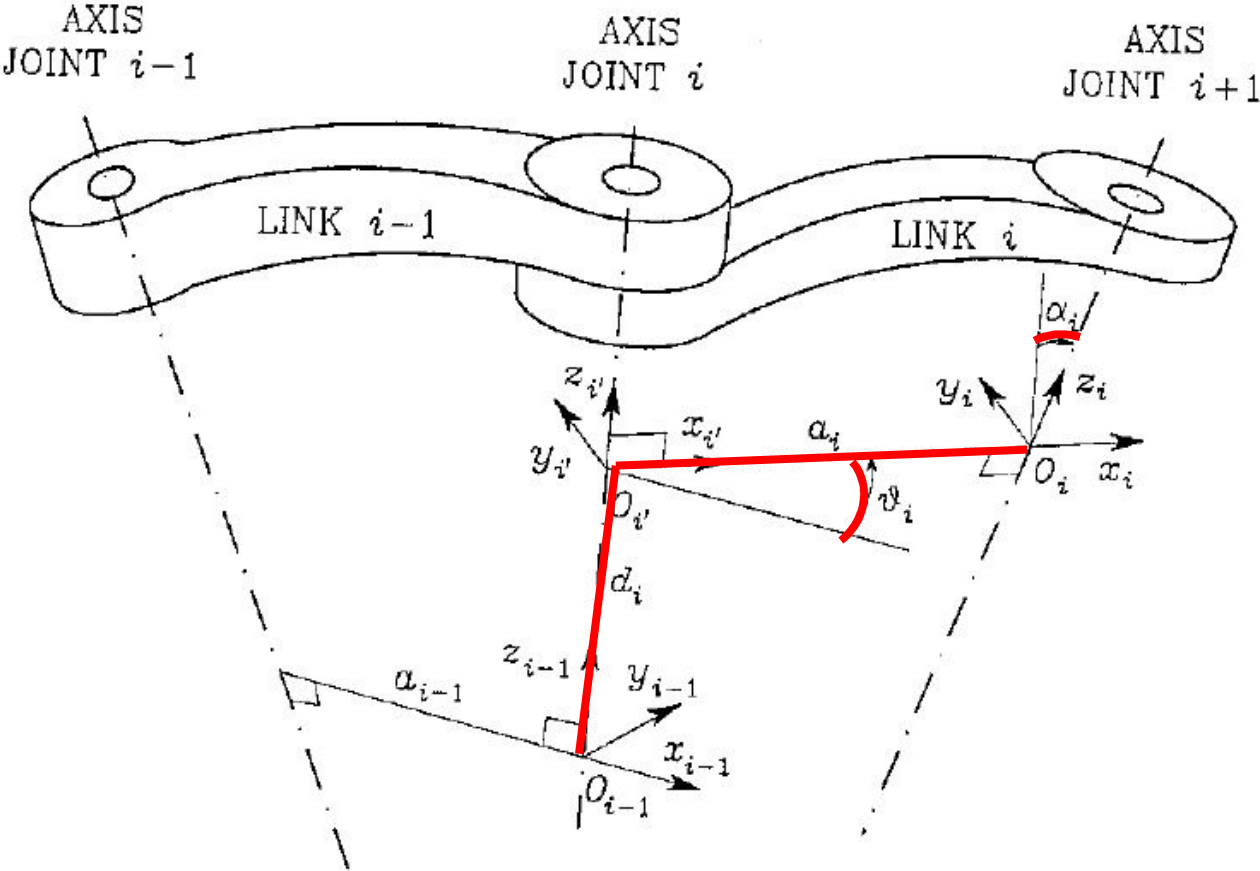
$d_i$  coordinate of  $O_{i'}$  along  $z_{i-1}$ ,

$\alpha_i$  angle between axes  $z_{i-1}$  and  $z_i$  about axis  $x_i$  to be taken positive when rotation is made counter-clockwise,

$\vartheta_i$  angle between axes  $x_{i-1}$  and  $x_i$  about axis  $z_{i-1}$  to be taken positive when rotation is made counter-clockwise.



# Denavit-Hartenberg Convention



# Denavit-Hartenberg Convention



- Parameters:
  - $a_i$  – length of the link
  - $d_i$  – displacement along z axis (how far from the same plane)
    - Only applies to *prismatic* joints
  - $\alpha_i$  – rotation along z axis
  - $\theta_i$  – rotation along x axis
    - only applies to *revolute* joints

# Denavit-Hartenberg Convention



$$A_{i'}^{i-1} = \begin{bmatrix} c_{\vartheta_i} & -s_{\vartheta_i} & 0 & 0 \\ s_{\vartheta_i} & c_{\vartheta_i} & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_i^{i'} = \begin{bmatrix} 1 & 0 & 0 & a_i \\ 0 & c_{\alpha_i} & -s_{\alpha_i} & 0 \\ 0 & s_{\alpha_i} & c_{\alpha_i} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_i^{i-1}(q_i) = A_{i'}^{i-1} A_i^{i'} = \begin{bmatrix} c_{\vartheta_i} & -s_{\vartheta_i} c_{\alpha_i} & s_{\vartheta_i} s_{\alpha_i} & a_i c_{\vartheta_i} \\ s_{\vartheta_i} & c_{\vartheta_i} c_{\alpha_i} & -c_{\vartheta_i} s_{\alpha_i} & a_i s_{\vartheta_i} \\ 0 & s_{\alpha_i} & c_{\alpha_i} & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Denavit-Hartenberg Convention



1. Find and number consecutively the joint axes; set the directions of axes  $z_0, \dots, z_{n-1}$ .
2. Choose the base frame by locating the origin on axis  $z_0$ ; axes  $x_0$  and  $y_0$  are chosen so as to obtain a right-handed frame.

Execute steps from **3** to **5** for  $i = 1, \dots, n - 1$ :

3. Locate the origin  $O_i$  at the intersection of  $z_i$  with the common normal to axes  $z_{i-1}$  and  $z_i$ . If axes  $z_{i-1}$  and  $z_i$  are parallel and joint  $i$  is revolute, then locate  $O_i$  so that  $d_i = 0$ ; if joint  $i$  is prismatic, locate  $O_i$  at a reference position for the joint range, e.g., a mechanical limit.
4. Choose axis  $x_i$  along the common normal to axes  $z_{i-1}$  and  $z_i$  with direction from joint  $i$  to joint  $i + 1$ .
5. Choose axis  $y_i$  so as to obtain a right-handed frame.

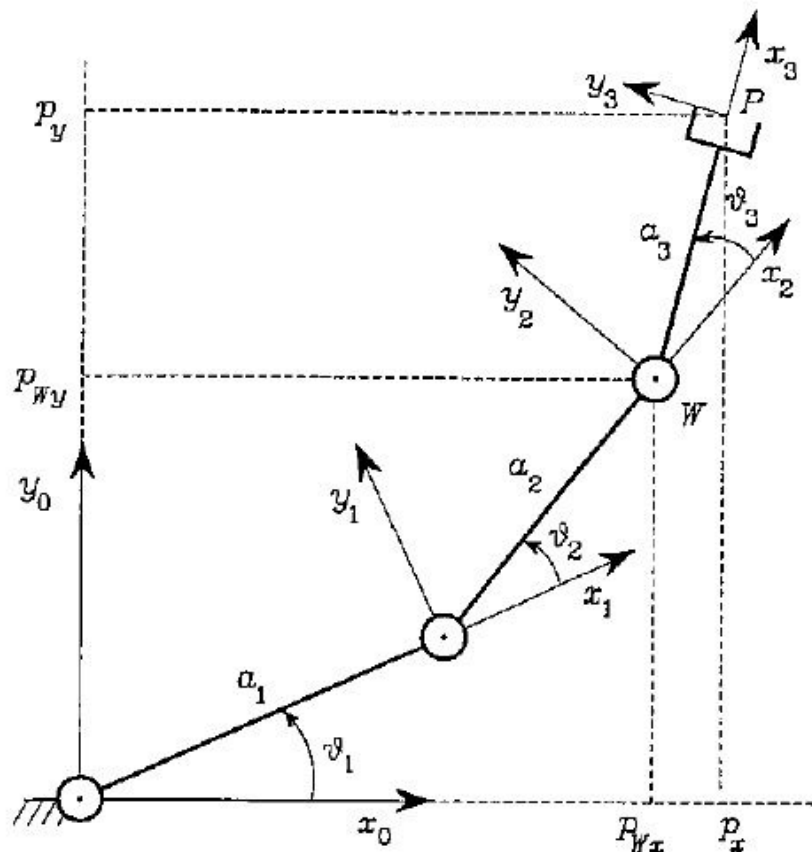
# Denavit-Hartenberg Convention



To complete:

6. Choose frame  $n$  with axis  $x_n$  normal to axis  $z_{n-1}$ ; if joint  $n$  is revolute, then align  $z_n$  with the direction of  $z_{n-1}$ .
7. For  $i = 1, \dots, n$ , form the table of parameters  $a_i, d_i, \alpha_i, \vartheta_i$ .
8. On the basis of the parameters in 7, compute the homogeneous transformation matrices  $A_i^{i-1}(q_i)$  for  $i = 1, \dots, n$ .
9. Compute the direct kinematics function  $T_n^0(\mathbf{q}) = A_1^0 \dots A_n^{n-1}$  that yields the position and orientation of frame  $n$  with respect to the base frame.

# Examples: Three-Link Planar Arm

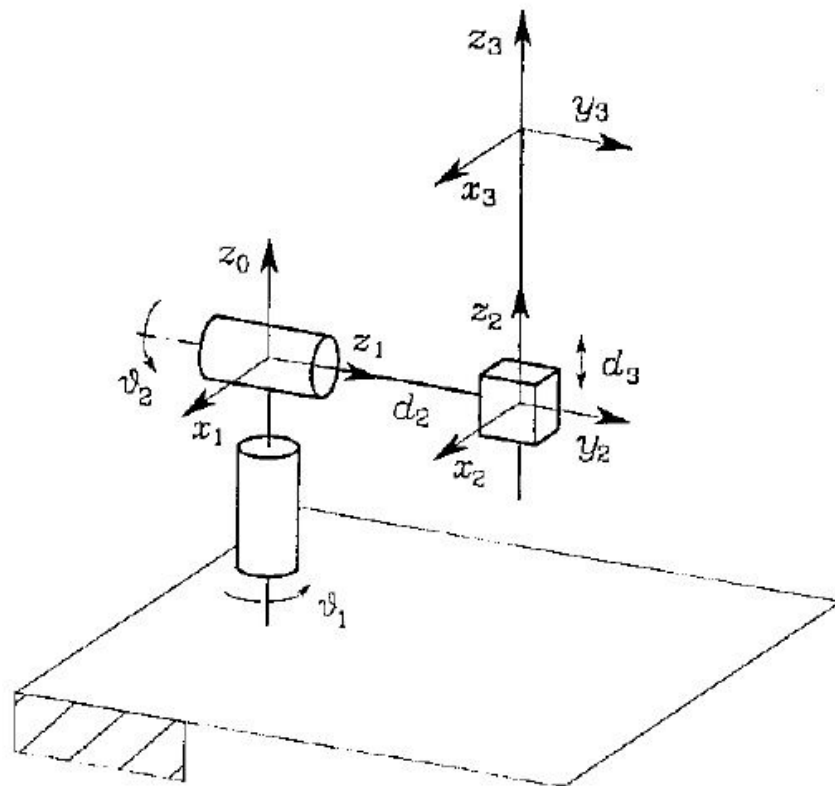


Link	$a_i$	$\alpha_i$	$d_i$	$\vartheta_i$
1	$a_1$	0	0	$\vartheta_1$
2	$a_2$	0	0	$\vartheta_2$
3	$a_3$	0	0	$\vartheta_3$

$$A_i^{i-1}(\vartheta_i) = \begin{bmatrix} c_i & -s_i & 0 & a_i c_i \\ s_i & c_i & 0 & a_i s_i \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad i = 1, 2, 3.$$

$$T_3^0(q) = A_1^0 A_2^1 A_3^2 = \begin{bmatrix} c_{123} & -s_{123} & 0 & a_1 c_1 + a_2 c_{12} + a_3 c_{123} \\ s_{123} & c_{123} & 0 & a_1 s_1 + a_2 s_{12} + a_3 s_{123} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Examples: Spherical Arm



Link	$a_i$	$\alpha_i$	$d_i$	$\vartheta_i$
1	0	$-\pi/2$	0	$\vartheta_1$
2	0	$\pi/2$	$d_2$	$\vartheta_2$
3	0	0	$d_3$	0

# Examples: Spherical Arm



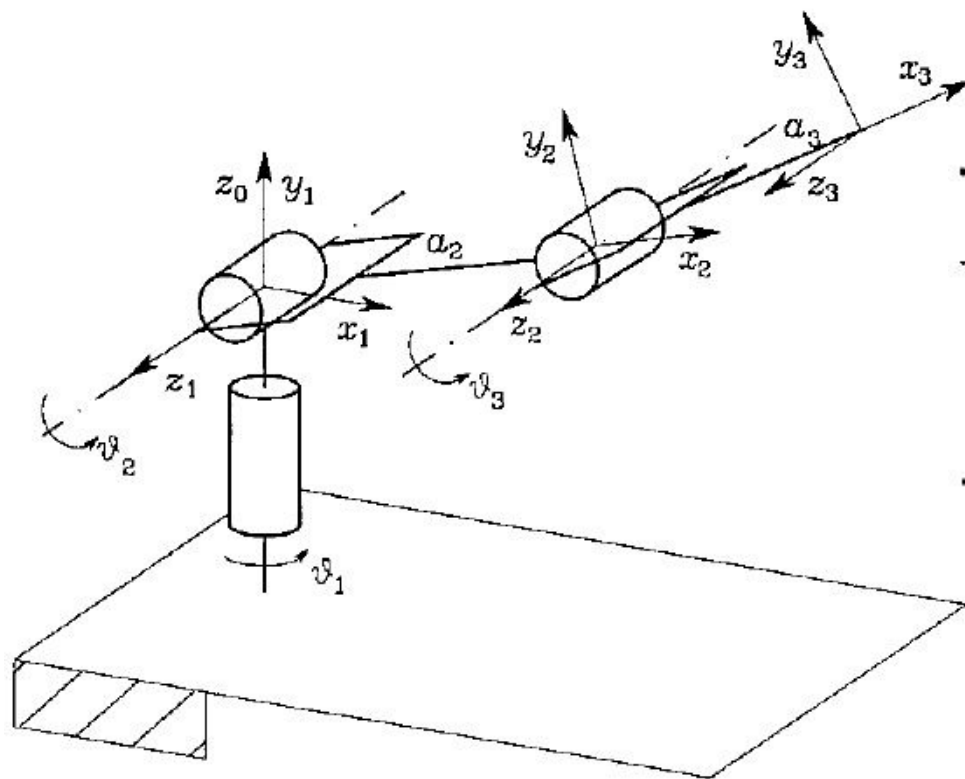
$$\mathbf{A}_1^0(\vartheta_1) = \begin{bmatrix} c_1 & 0 & -s_1 & 0 \\ s_1 & 0 & c_1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \mathbf{A}_2^1(\vartheta_2) = \begin{bmatrix} c_2 & 0 & s_2 & 0 \\ s_2 & 0 & -c_2 & 0 \\ 0 & 1 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{A}_3^2(d_3) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{T}_3^0(\mathbf{q}) = \mathbf{A}_1^0 \mathbf{A}_2^1 \mathbf{A}_3^2 = \begin{bmatrix} c_1 c_2 & -s_1 & c_1 s_2 & c_1 s_2 d_3 - s_1 d_2 \\ s_1 c_2 & c_1 & s_1 s_2 & s_1 s_2 d_3 + c_1 d_2 \\ -s_2 & 0 & c_2 & c_2 d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



# Examples: Anthropomorphic Arm



Link	$a_i$	$\alpha_i$	$d_i$	$\vartheta_i$
1	0	$\pi/2$	0	$\vartheta_1$
2	$a_2$	0	0	$\vartheta_2$
3	$a_3$	0	0	$\vartheta_3$

# Examples: Anthropomorphic Arm

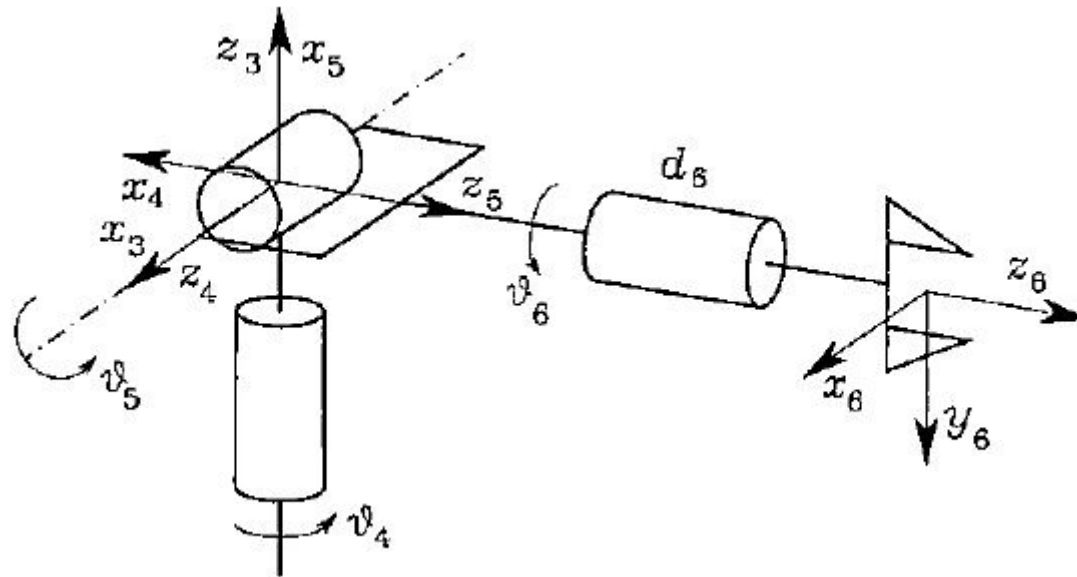


$$A_1^0(\vartheta_1) = \begin{bmatrix} c_1 & 0 & s_1 & 0 \\ s_1 & 0 & -c_1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_i^{i-1}(\vartheta_i) = \begin{bmatrix} c_i & -s_i & 0 & a_i c_i \\ s_i & c_i & 0 & a_i s_i \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad i = 2, 3$$

$$T_3^0(q) = A_1^0 A_2^1 A_3^2 = \begin{bmatrix} c_1 c_{23} & -c_1 s_{23} & s_1 & c_1 (a_2 c_2 + a_3 c_{23}) \\ s_1 c_{23} & -s_1 s_{23} & -c_1 & s_1 (a_2 c_2 + a_3 c_{23}) \\ s_{23} & c_{23} & 0 & a_2 s_2 + a_3 s_{23} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Examples: Spherical Wrist



Link	$a_i$	$\alpha_i$	$d_i$	$\vartheta_i$
4	0	$-\pi/2$	0	$\vartheta_4$
5	0	$\pi/2$	0	$\vartheta_5$
6	0	0	$d_6$	$\vartheta_6$

# Examples: Spherical Wrist



$$A_4^3(\vartheta_4) = \begin{bmatrix} c_4 & 0 & -s_4 & 0 \\ s_4 & 0 & c_4 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad A_5^4(\vartheta_5) = \begin{bmatrix} c_5 & 0 & s_5 & 0 \\ s_5 & 0 & -c_5 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

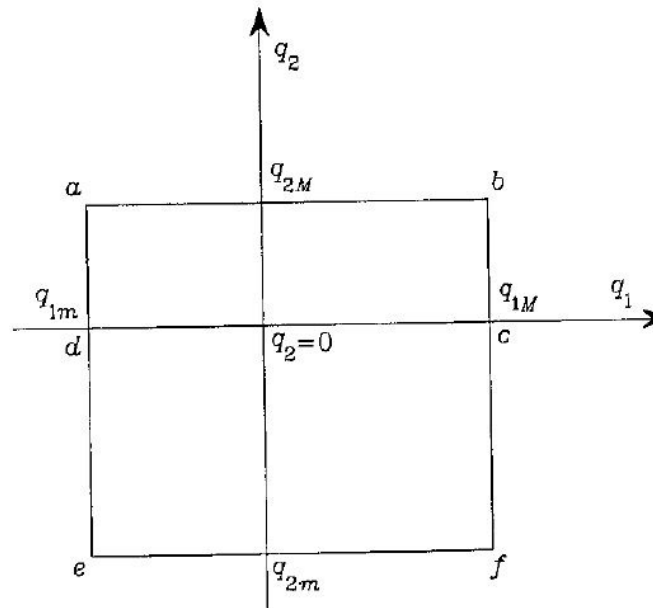
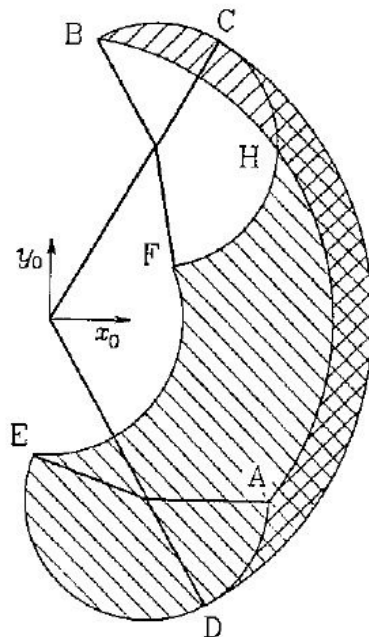
$$A_6^5(\vartheta_6) = \begin{bmatrix} c_6 & -s_6 & 0 & 0 \\ s_6 & c_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}.$$

$$T_6^3(q) = A_4^3 A_5^4 A_6^5 = \begin{bmatrix} c_4 c_5 c_6 - s_4 s_6 & -c_4 c_5 s_6 - s_4 c_6 & c_4 s_5 & c_4 s_5 d_6 \\ s_4 c_5 c_6 + c_4 s_6 & -s_4 c_5 s_6 + c_4 c_6 & s_4 s_5 & s_4 s_5 d_6 \\ -s_5 c_6 & s_5 s_6 & c_5 & c_5 d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Workspace Considerations



- *Operational space* – set of all configurations a end-effector can achieve
  - Orientation and position
- *Joint space* – possible values the joints can take



# Workspace Considerations



- *Accuracy* – Deviation between assigned position and actual position of end-effector
- *Repeatability* – Ability to return to previous position
- *Kinematic Redundancy* – Number of degrees greater than the number of variables necessary to describe task
  - Multiple configurations to reach same end-effector position